

## ***TPS61040 Inverter Design***

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### **ABSTRACT**

Although designed to be a positive voltage boost converter, the TPS61040 can be configured as an inverting converter using an OPA348 operational amplifier or equivalent to invert the feedback signal.

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Although designed to be a positive voltage boost converter, the TPS61040 can be configured as an inverting converter. The application section of the TPS61040 data sheet (Figure 19) shows an implementation using a discrete charge pump to produce a positive voltage rail and an auxiliary negative rail with the same magnitude as the positive rail. However, the negative rail produced by the charge pump is outside of the control loop, so its load regulation is dependent on the positive rail's regulation. This type of tracking regulation is acceptable when dual rail ICs require approximately the same amount of current into/out of each rail. Using an OPA348 operational amplifier or equivalent, this configuration is modified to provide a negative rail and an optional auxiliary positive rail, as shown in Figure 1. Depending on the operational amplifier's operating voltage, the auxiliary positive rail could be used to power the operational amplifier. The operational amplifier inverts the feedback signal so that it can be tied to the FB pin of the TPS61040. Resistors R3 and R1 are sized to give the operational amplifier an inverting gain that converts the negative rail voltage to 1.233 V. Capacitor C2 is required to stabilize the operational amplifier. Resistor R2 is used to prevent a large current spike through the IC's switch when D3 turns on.

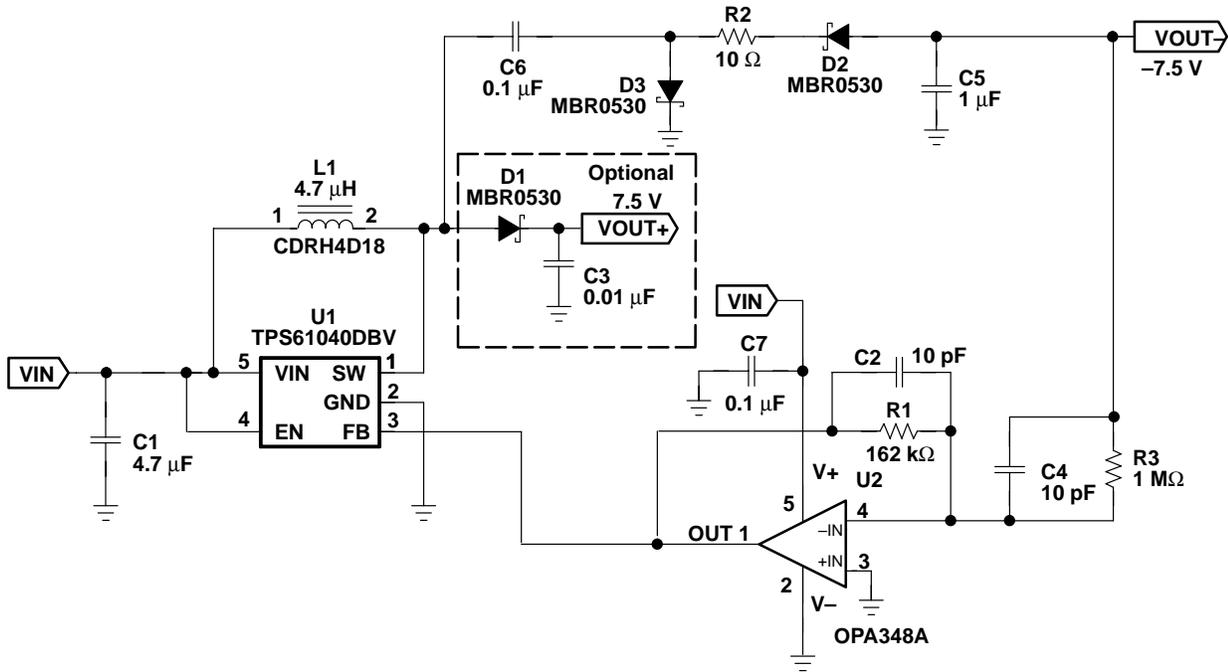


Figure 1. Charge Pump Inverter

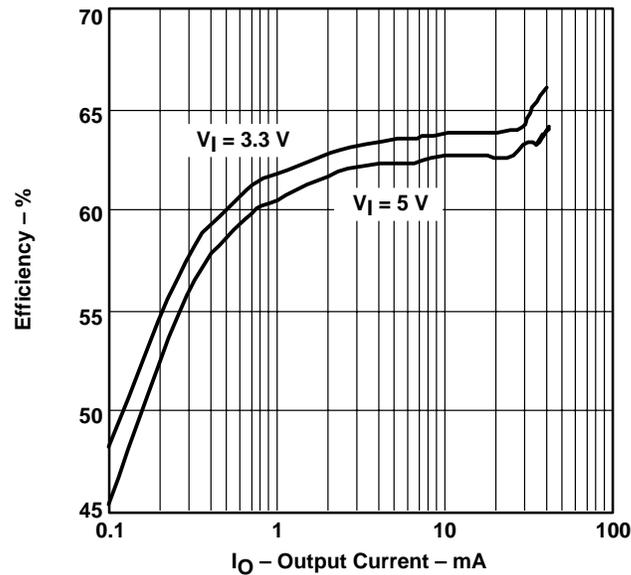


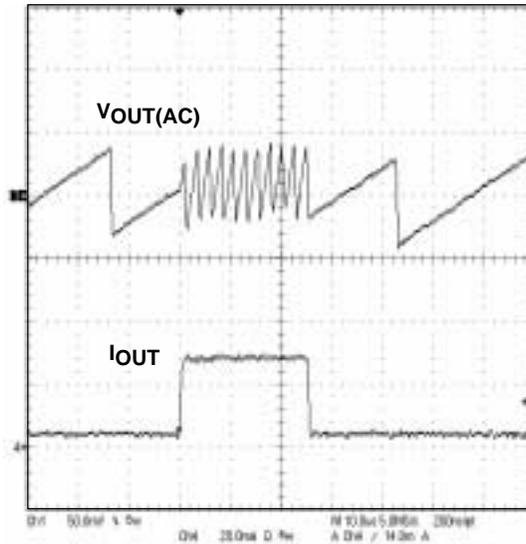
Figure 2. Efficiency for TPS61040 Charge Pump Inverter Using CDRH4D18-4R7

Assuming 65% efficiency for the charge pump design, the TPS61040 data sheet equation for computing maximum load (shown below) predicts maximum load currents of 54 mA and 81 mA for  $V_{IN} = 3.3\text{ V}$  and  $V_{IN} = 5.0\text{ V}$ , respectively. The measured load currents at the point where the design enters continuous conduction mode are 50 mA and 75 mA.

$$I_{LMAX} = \eta \times \frac{V_{INmin} \times I_P}{2 \times (V_O + V_{DIODE})}$$

where  $\eta$  is the estimated efficiency.

Load transient results with  $V_{IN} = 5.0\text{ V}$  and  $I_{OUT}$  transitioning from 1 mA to 25 mA are shown in Figure 3.



**Figure 3. Load Transient Response of the TPS61040 Charge Pump Inverter**

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